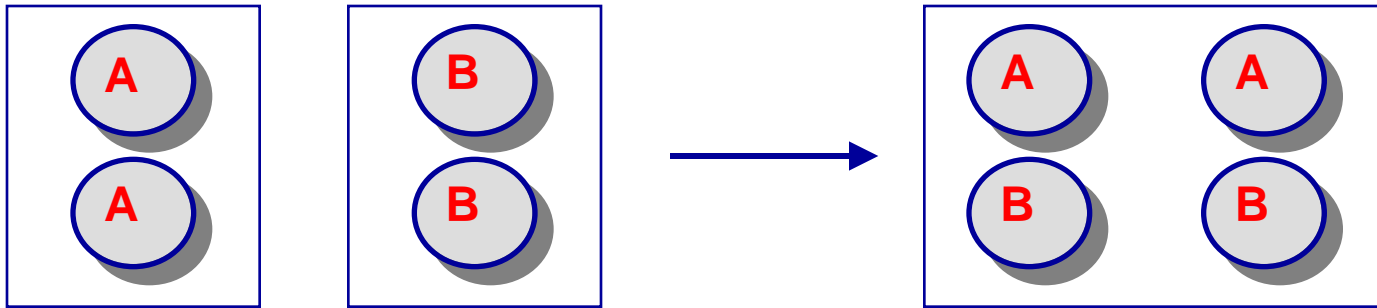


# THE FLORY PARAMETER



$$w_{AB} = \frac{1}{2}(w_{AA} + w_{BB}) - w_{AB}$$

Energy change per AB contact

$$\bar{A} = w_{AB} z/RT$$

Energy difference (/RT) between an A molecule  
Surrounded by other A's, and one surrounded by B's

$$H_m = n_A \bar{A} (RT)$$

Heat of mixing (multiply energy difference  
By the number of AB contacts)

# FREE ENERGY OF MIXING- FLORY - HUGGINS THEORY

$$G_m = H_m - T S$$

$$\frac{G_m}{RT} = \boxed{n_A \ln \phi_A + n_B \ln \phi_B} + \boxed{\chi_{AB} n_A \phi_B}$$

ENTROPIC TERM

ENTHALPIC TERM

The diagram illustrates the Flory-Huggins equation for the free energy of mixing. The equation is presented as  $\frac{G_m}{RT} = \boxed{n_A \ln \phi_A + n_B \ln \phi_B} + \boxed{\chi_{AB} n_A \phi_B}$ . The first term, enclosed in a dashed purple box, is identified by a purple arrow as the 'ENTROPIC TERM'. The second term, also enclosed in a dashed purple box, is identified by a purple arrow as the 'ENTHALPIC TERM'.

# RELATIONSHIP BETWEEN AND SOLUBILITY PARAMETERS

The expressions for the heat of mixing are equivalent

$$H_m = N_s \quad p (RT \quad )$$

$$H_m = V_m (n_s + n_p) \quad ( \quad_s - \quad_p )^2 \quad_s \quad_p$$

**Using**  $\quad_s = \frac{n_s V_s}{V_m}$

**Then**  $= \frac{V_s}{RT} ( \quad_s - \quad_p )^2$

**But, experimentally for solutions (not blends)**

$$\sim 0.34 + \frac{V_s}{RT} ( \quad_s - \quad_p )^2$$

# WHY MOST SIMPLE HYDROCARBON POLYMERS DON'T MIX

$$\frac{G_m}{RT} = n_A \ln \phi_A + n_B \ln \phi_B + n_A \chi_B$$

Combinatorial entropy  
- Small

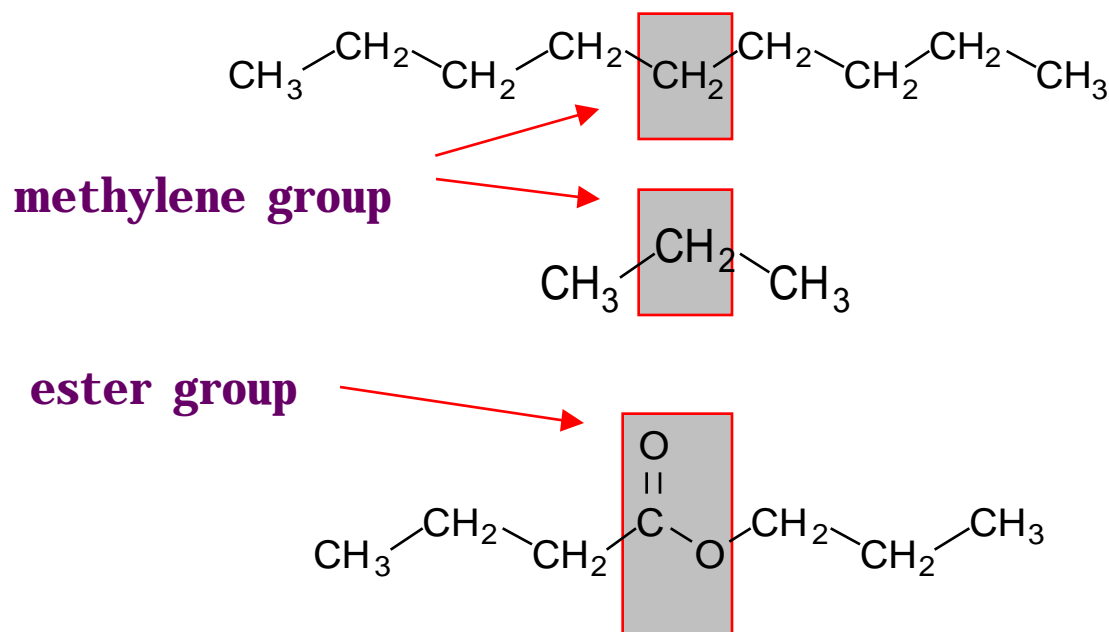
Interaction term  
- Positive

$$= \frac{V_{ref}}{RT} [\phi_A - \phi_B]^2$$

To obtain a miscible system we must  
Have specific interactions

# SOLUBILITY PARAMETERS OF POLYMERS

- Cannot be obtained from energy of vaporization measurements
- Use group contributions



# **SOME LIMITATIONS OF THE FLORY – HUGGINS THEORY**

- 1. BASED ON A LATTICE MODEL THAT USES  
VARIOUS APPROXIMATIONS IN THE  
“COUNTING” PROCESS**
- 2. IGNORES "FREE VOLUME"**
- 3. ASSUMES RANDOM MIXING OF CHAINS  
IN CALCULATING THE ENTROPY AND  
SEGMENTS IN CALCULATING THE ENTHALPY**
- 4. STRICTLY, ONLY APPLIES TO NON -  
POLAR MOLECULES**
- 5. ONLY ACCOUNTS FOR COMBINATORIAL  
ENTROPY**

# PHASE BEHAVIOUR

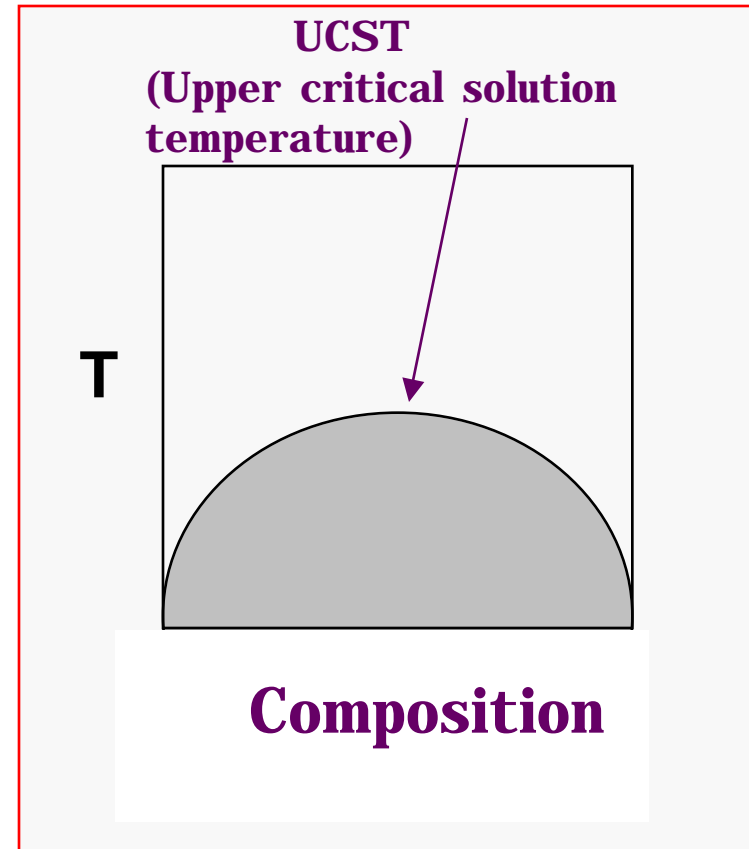
RECALL THAT

$$= \frac{V_s}{RT} (\phi_s - \phi_p)^2$$

Hence increases with decreasing temperature

Accordingly, one might expect that as the temperature of a solution (or blend) is lowered, there comes a point where the free energy becomes positive and phase separation occurs.

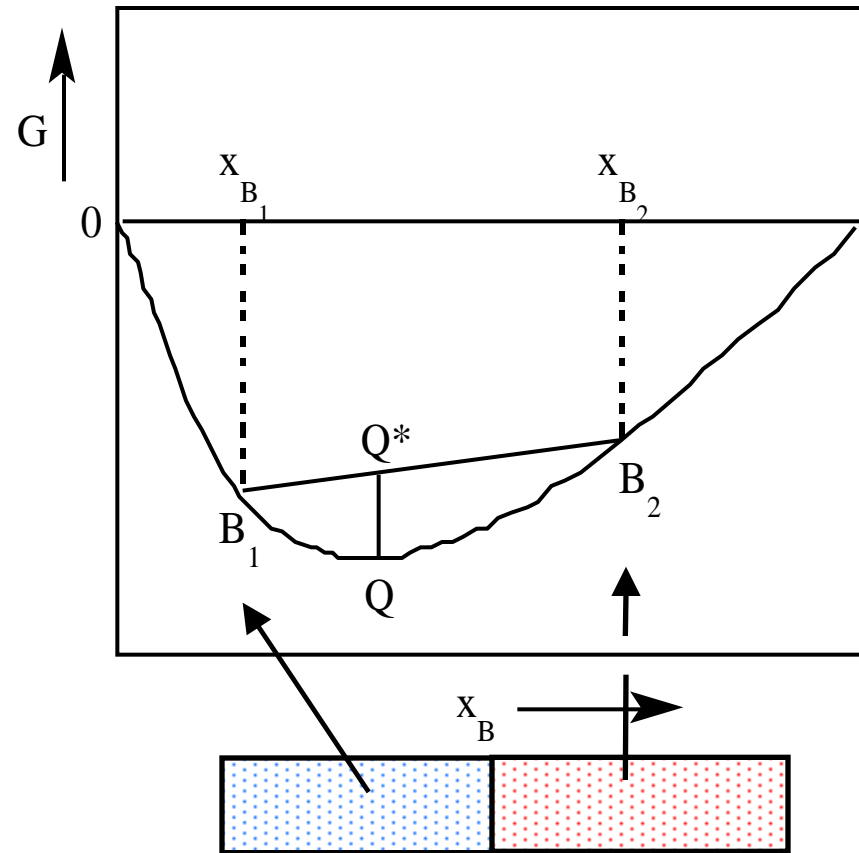
Schematically, the phase diagram would look like



# PHASE BEHAVIOUR

However, the free energy does not have to be positive in order to have phase separation !!!

The shape of the free energy / Composition curve is crucial

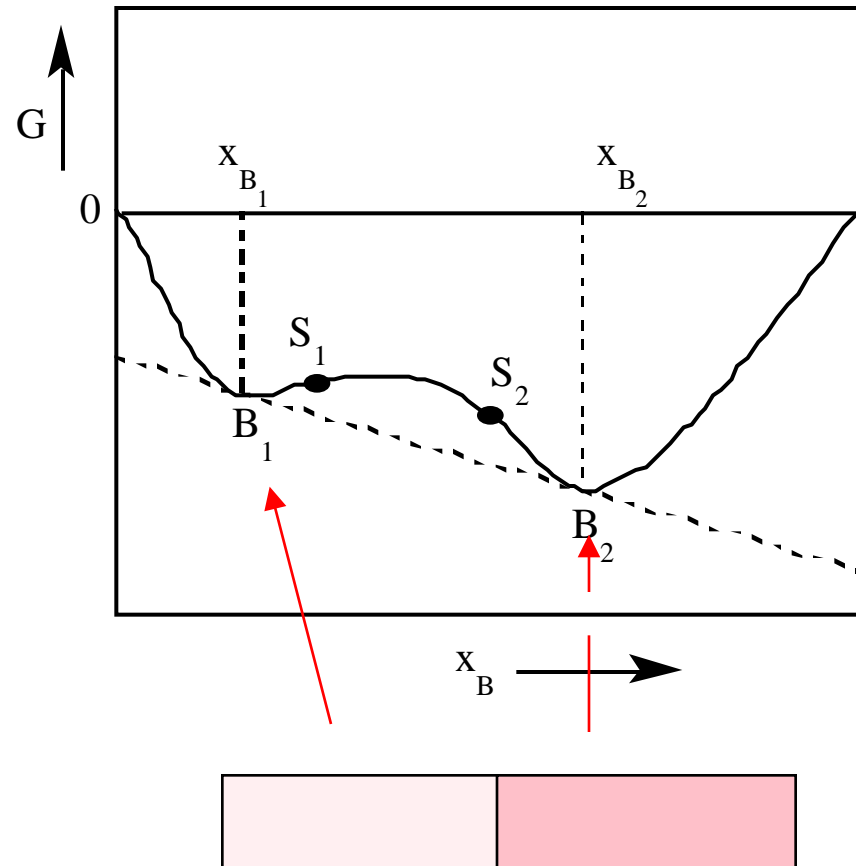


IF THE BARRIER IS REMOVED, WOULD THE TWO SOLUTIONS MIX?



# EVEN MORE PHASE BEHAVIOUR

WHAT IF THE FREE ENERGY CURVE LOOKED LIKE THIS ?

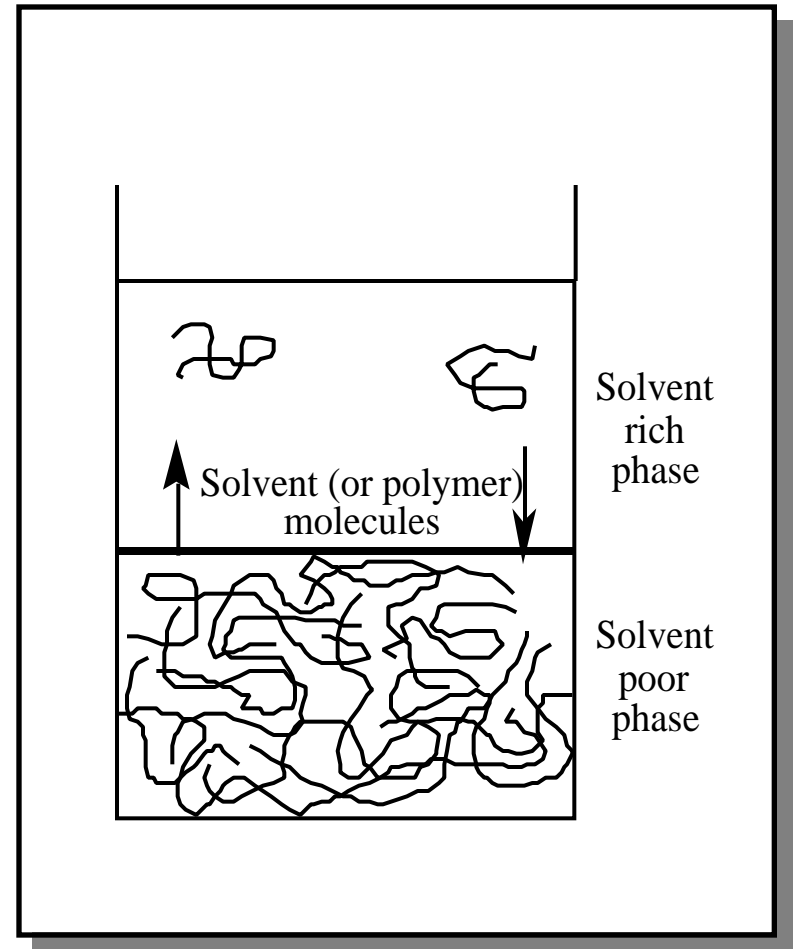


# CHEMICAL POTENTIAL

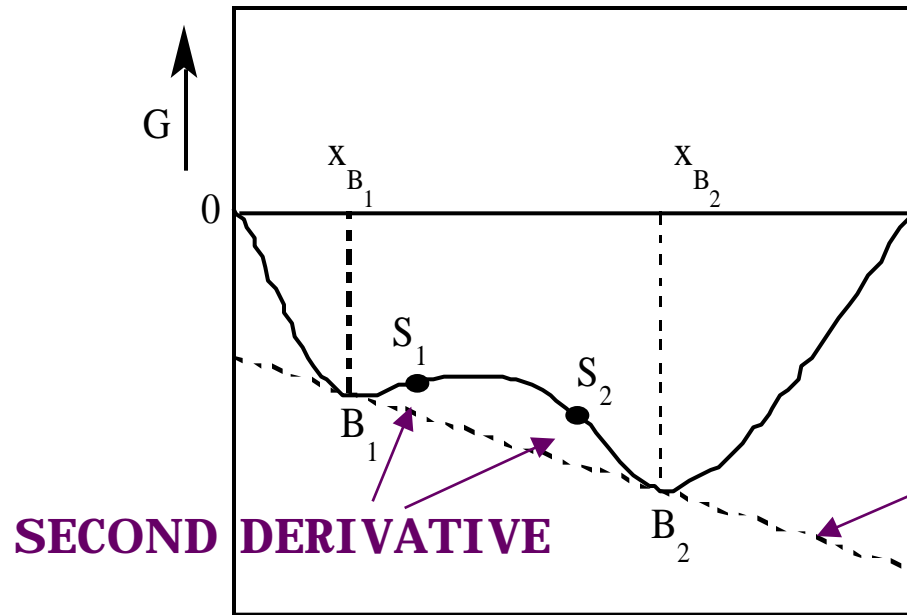
FROM THE FLORY - HUGGINS  
EQUATION;

$$\frac{\mu_s - \mu_s^0}{RT} = \frac{(\Delta G_m/RT)}{N_s}$$

$$= \ln(1 - \phi_p) + \left(1 - \frac{1}{M}\right) \phi_p + \frac{2}{M} \phi_p^2$$

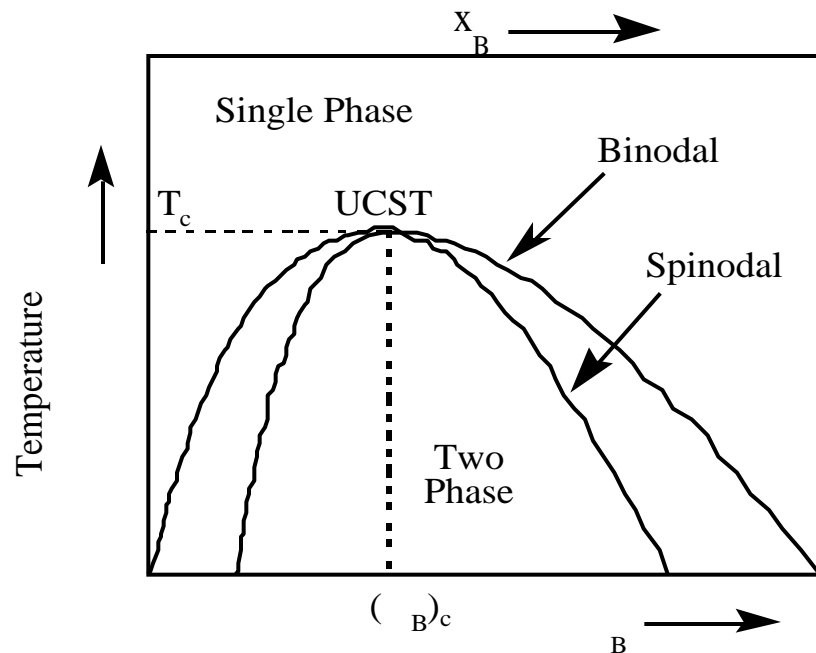


# CALCULATING A PHASE DIAGRAM



FREE ENERGY CURVE AT A GIVEN  $T$

FIRST DERIVATIVE  
OF FREE ENERGY  
WITH RESPECT TO  
COMPOSITION  
(chemical potential)



COLLECTING ALL THE  
POINTS FROM FREE  
ENERGY CURVES  
CALCULATED AT  
VARIOUS TEMPERATURES

# THE CRITICAL VALUE OF

DEFINED BY

$$\frac{\partial^2 (G_m)_s}{\partial c^2} = 0$$

$$\frac{\partial^3 (G_m)_s}{\partial c^3} = 0$$

However, we can also start from  
The chemical potential and differentiate  
successively to obtain

$$\frac{1}{(1 - p)} - 1 - \frac{1}{M} - 2p = 0$$

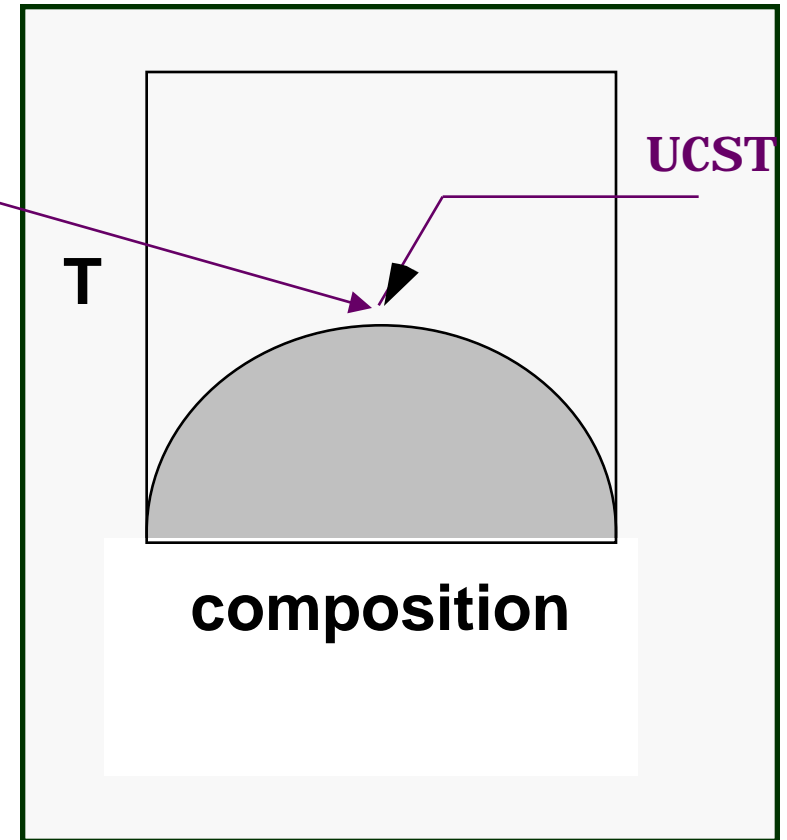
$$\frac{1}{(1 - p)^2} - 2 = 0$$

FOR SOLUTIONS

$$c = \frac{1}{2} \left( 1 + \frac{1}{M_s^{1/2}} \right)^2 \sim 0.5$$

FOR BLENDS

$$c = \frac{1}{2} \left( \frac{1}{M_A^{1/2}} + \frac{1}{M_B^{1/2}} \right)^2 \sim \text{very small}$$



# CRITICAL VALUE OF THE SOLUBILITY PARAMETER DIFFERENCE

RECALL THAT

$$\sim 0.34 + \frac{V_s}{RT} (\chi_s - \chi_p)^2$$

THEN IF  $V_s / RT \sim 1/6$

$$\chi_s - \chi_p \sim \{(0.5 - 0.34) 6\}^{1/2} \sim 0.98$$

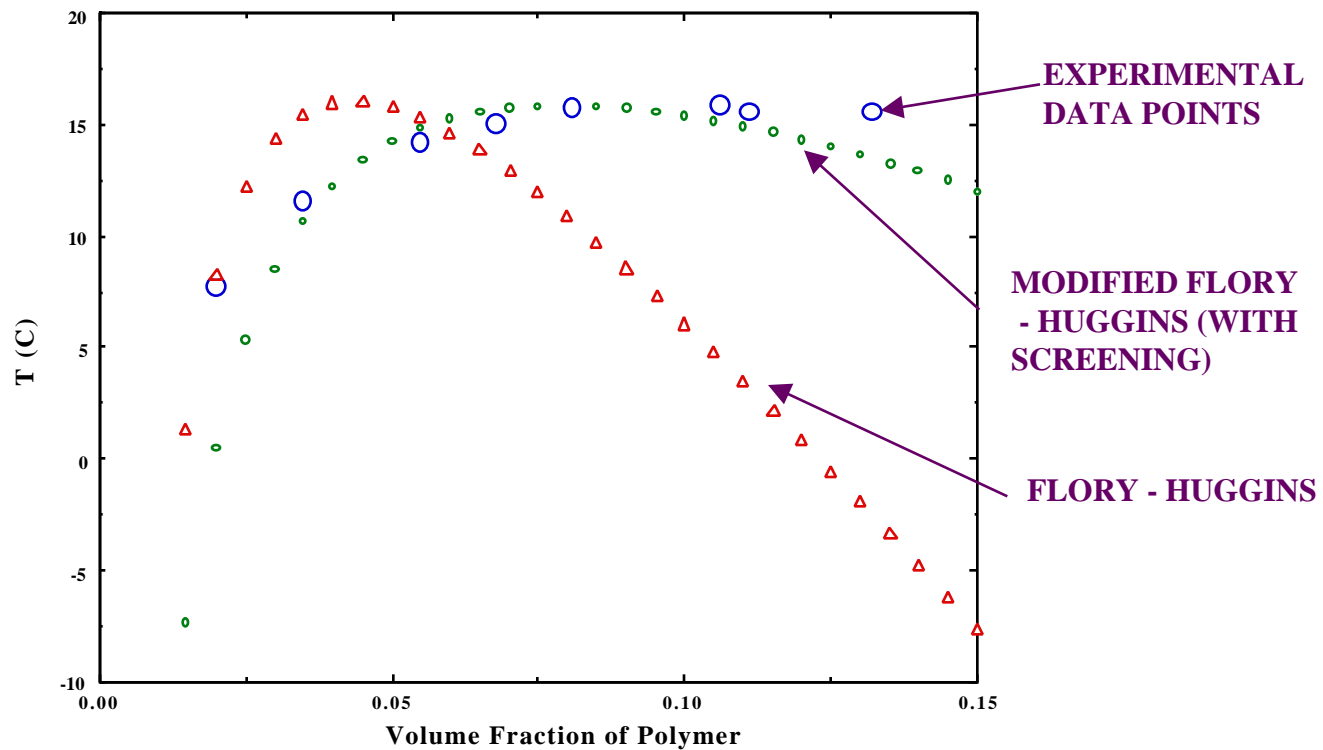
HENCE

$$\chi_s - \chi_p < 1$$

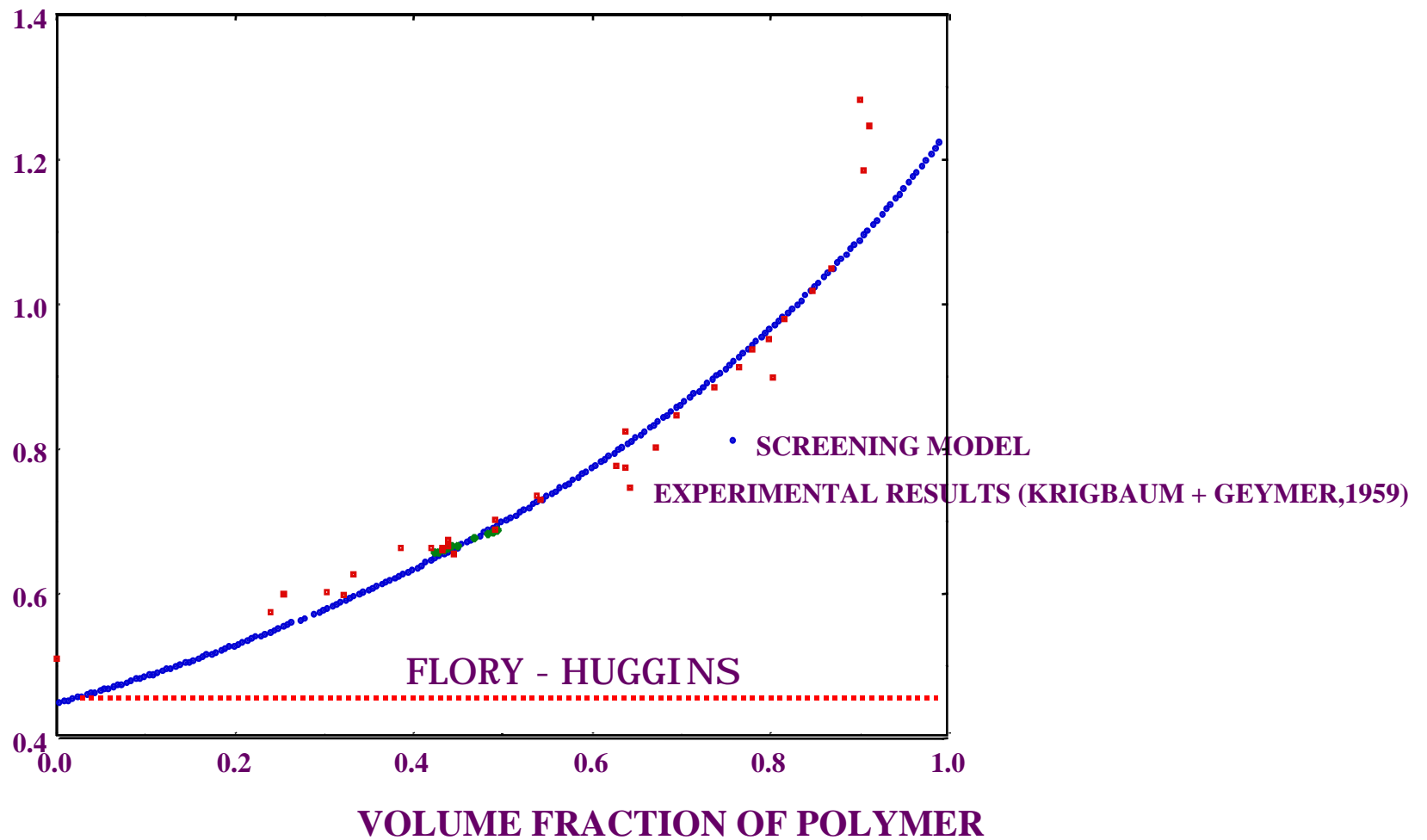
OR, MORE PRECISELY

$$c = \pm 1$$

# SPINODAL FOR POLYSTYRENE - CYCLOHEXANE

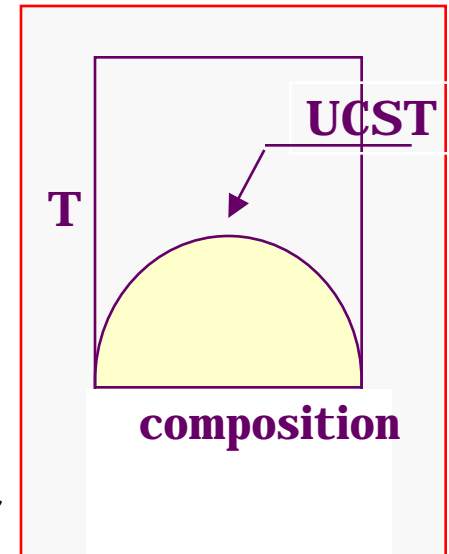


# VALUES OF $\chi_1$ FOR SOLUTIONS OF POLYSTYRENE IN CYCLOHEXANE

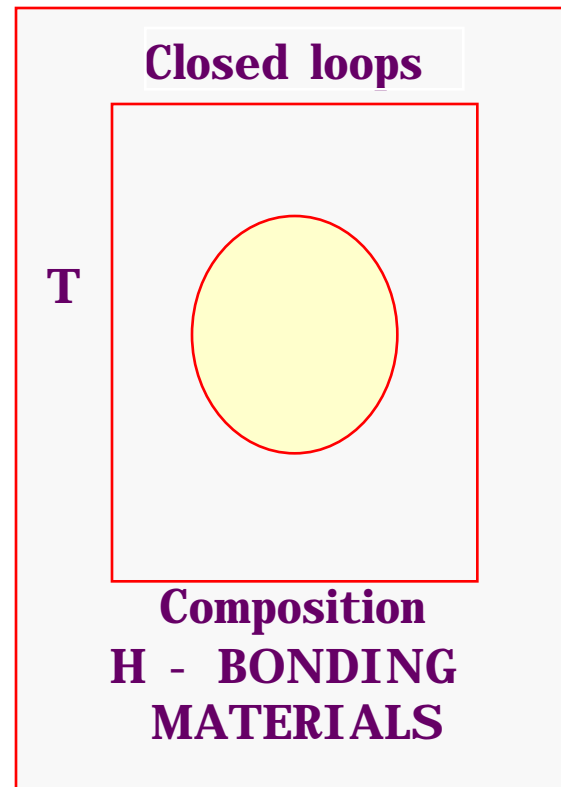
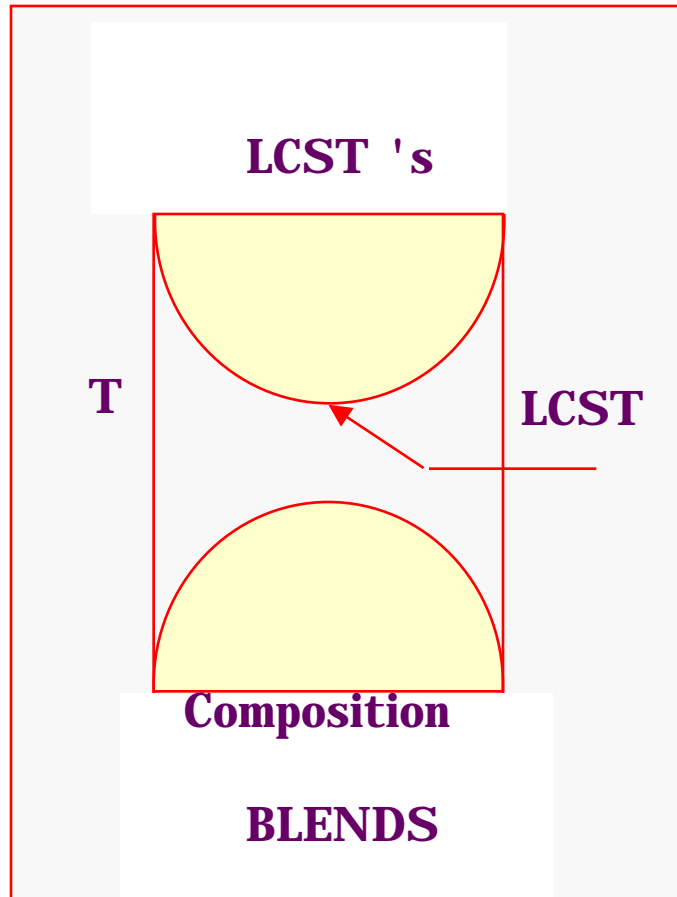


# PREDICTIONS OF SIMPLE MODEL

1. Most polymers won't mix
2. UCST phase behaviour

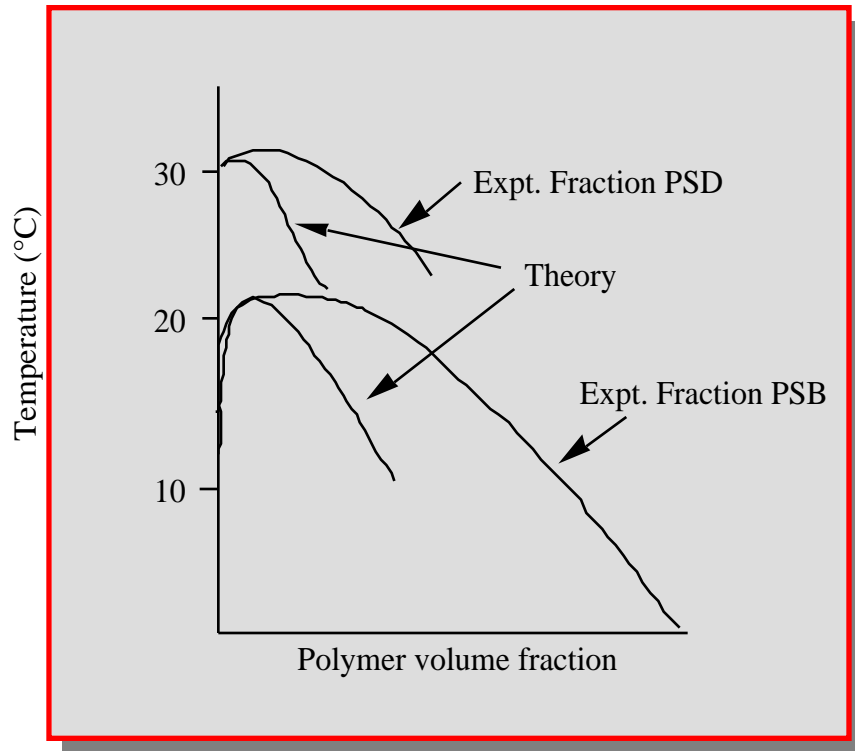


## OBSERVED BEHAVIOUR

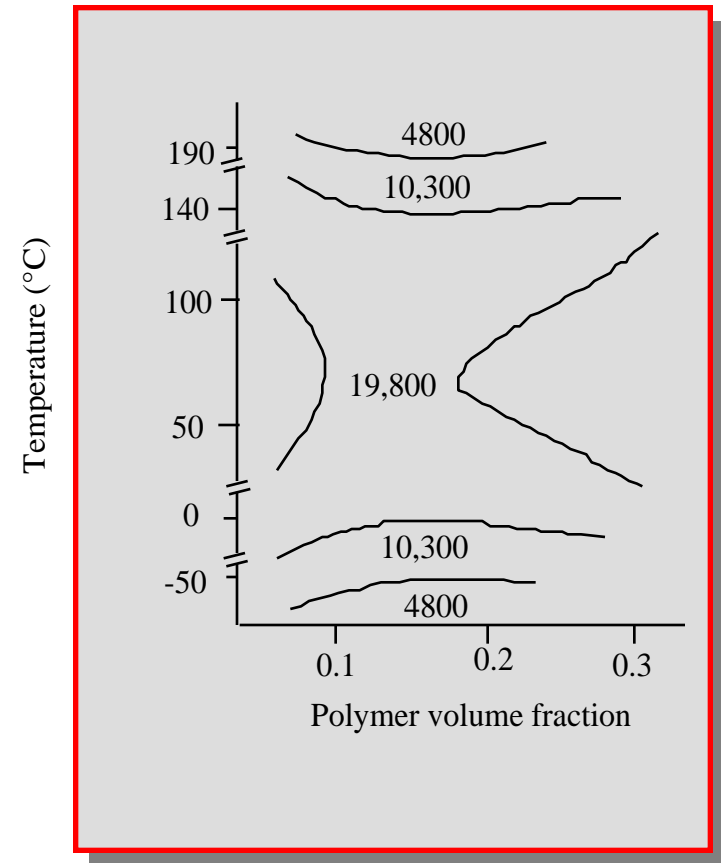




# COMPARISON TO EXPERIMENT



**SHULTZ AND FLORY**



**SIOW ET AL**

# THE TEMPERATURE

